Occupant Trajectory

Distance Traveled by an Ejected Vehicle Occupant or Component

A number of analytical relationships have been applied in the past for the purpose of interpreting the travel distances of ejected vehicle occupants or components. In the following, the related assumptions and the derivations of several such relationships are outlined. A summary comparison of the analytical relationships is presented in

Table 13. The analytical basis for a general-case analytical approach with an iterative solution procedure, which has been developed by McHenry Software, Inc., as the LAUNCH routine, is then briefly outlined.

Simple Ballistic Trajectory

An oversimplified analytical relationship that has sometimes been used to approximate the <u>minimum</u> speed of an ejected occupant or component is based on a ballistic trajectory with the following inherent assumptions:

- 1. The optimum launch angle (i.e., 45°) to determine the minimum speed for a given travel distance,
- 2. A landing at the same elevation as the launch, and
- 3. No movement on the ground after the landing.

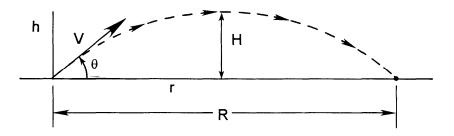


Figure 67 Simple Ballistic Trajectory

The assumed behavior is depicted in Figure 67 and the cited relationship is derived as follows:

$$h = (V \sin \theta) t - \frac{1}{2} gt^{2}$$
(1)

$$h = 0 \text{ when } t = 0, \text{ and when } t = \frac{2V \sin \theta}{g}.$$

$$r = (V \cos \theta) t$$
(2)

$$P = \frac{2V^{2}}{g} \cos \theta \sin \theta$$
(3)

$$R = \frac{2V^2}{g} \cos\theta \sin\theta$$
(3)

$$\frac{dR}{d\theta} = \frac{2V^2}{g} \left(\cos^2 \theta - \sin^2 \theta \right)$$
For $\frac{dR}{d\theta} = 0, \ \theta = 45^{\circ}$

$$R = \frac{V^2}{g}$$
(5)

$$V_{\min} = \sqrt{Rg} \quad FT/SEC$$
(6)
= 5.675 $\sqrt{R} \quad FT/SEC$

$$V_{\min} = 3.869 \sqrt{R} \text{ MPH}$$
(7)

where R = Feet.

The unrealistic nature of equation (7) becomes more apparent when the corresponding maximum elevation is determined.

From Equation (1),

$$\frac{dh}{dt} = V \sin \theta - gt$$
(8)
For $\frac{dh}{dt} = 0, t = \frac{V \sin \theta}{g}$
Evaluation of equation (1) at
 $t = \frac{V \sin \theta}{g}$ yields :
 $H = \frac{V^2 \sin^2 \theta}{2g}$
(9)
From equations (3) and (9), for $\theta = 45^\circ$:
 $H = 0.25R$
(10)

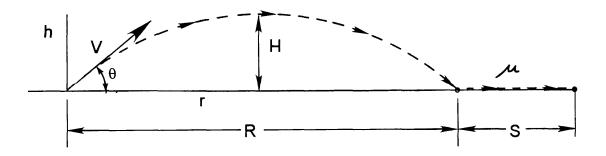


Figure 68 Ballistic Trajectory Followed by Sliding

Ballistic Trajectory Followed by Sliding

If it is assumed that the motion continues after landing (as depicted in **Figure 68**), with an average drag force equal to μ Mg, the following relationships can be developed:

$$R + S = \frac{2V^2}{g} \left(\sin \theta \cos \theta \right) + \frac{V^2 \cos^2 \theta}{2\mu g}$$
(11)

$$\frac{d(R + S)}{d\theta} = \frac{2V^2}{g} \left(\cos^2 \theta - \sin^2 \theta \right) - \frac{V^2}{\mu g} \left(\cos \theta \sin \theta \right)$$
(12)

The range (R + S) has a maximum value when $\frac{d(R + S)}{d\theta} = 0$,

which occurs for the following value of θ :

$$\cos^2\theta - \sin^2\theta - \frac{\cos\theta\sin\theta}{2\mu} = 0$$
(13)

$$\cos 2\theta - \frac{\sin 2\theta}{4\mu} = 0 \tag{14}$$

$$\theta = \frac{1}{2} \arctan \left(4\mu\right) \tag{15}$$

Using the following trigonometric relationships and Equation (15), Equation (11) can be solved for the required launch speed:

$$\cos^2 \theta = \frac{\left(1 + \cos 2\theta\right)}{2} \tag{16}$$

$$\sin \theta \cos \theta = \frac{\sin 2\theta}{2} \tag{17}$$

$$\tan \theta = \frac{\sin 2\theta}{(1 + \cos 2\theta)} \tag{18}$$

$$V = \sqrt{g(R + S) \tan \theta} \quad FT/SEC$$
(19)

$$V = 3.869 \quad \sqrt{(R + S) \tan \theta} \quad MPH$$

$$+S - Feet$$
(20)

Where R+S = Feet

Note that if $\mu \rightarrow \infty$, $\theta = 45^{\circ}$, S = 0,

and the results will be identical with Case 1 (simple Ballistic Trajectory).

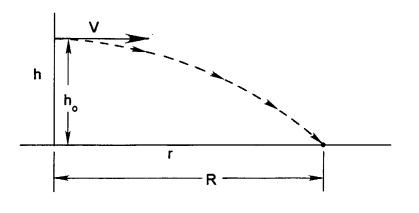


Figure 69 Simple Horizontal Launch

Simple Horizontal Launch

An oversimplified analytical relationship that has sometimes been used to approximate the <u>maximum</u> speed of an ejected occupant or component is based on a horizontal launch with the assumption of no movement on the ground after landing. The assumed behavior is depicted in **Figure 69**.

$$h = h_o - \frac{1}{2}gt^2 \tag{21}$$

For h = 0, t =
$$\sqrt{\frac{2H_0}{g}}$$
 (22)
R = Vt = V $\sqrt{\frac{2H_0}{g}}$ (23)

$$R = Vt = V \sqrt{\frac{2\Pi_0}{g}}$$

Solving for V,

$$V = R \sqrt{\frac{g}{2h_0}} FT/SEC$$
(24)

$$V = \frac{2.736R}{\sqrt{h_o}} MPH$$
(25)

where R, $h_o = Feet$

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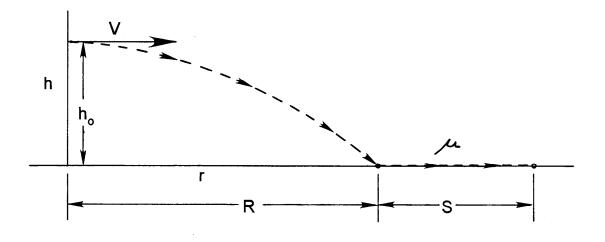


Figure 70 Horizontal Launch Followed by Sliding

Horizontal Launch Followed by Sliding

If it is assumed that the motion continues after landing (as depicted in **Figure 70**), with an average drag force equal to μ Mg, the following relationships can be developed:

$$R + S = V \sqrt{\frac{2h_0}{g}} + \frac{V^2}{2\mu g}$$
(26)

Solution of equation (26) for V yields :

$$V = -\mu \sqrt{2h_0 g} + \sqrt{2\mu g \left(\mu h_0 + R + S\right)} FT/SEC$$
(27)

$$V = 5.4716 \left\{ -\mu \sqrt{h_0} + \sqrt{\mu (\mu h_0 + R + S)} \right\} MPH$$
(28)

where R, S, $h_o = Feet$

| | 1 | 2 | 3 | 4 | |
|----------------------------------|-----------------------------------|---|--------------------------------|--|---------|
| Quantity | Simple Ballistic Trajectory | Ballistic Trajectory Followed by Sliding | Simple Horizontal Launch | Horizontal Launch Followed by Sliding | UNITS |
| Total Horizontal | _ | | | | |
| Travel | <u> </u> | R+S | R | R+S | FEET |
| Terrain Surface Deceleration | œ | μ | œ | μ | G Units |
| Elevation of Launch | 0 | 0 | h ₀ | h _o | Feet |
| Angle of Launch, θ | 45° | ½ arctan (4µ) | 0.0° | 0.0° | Degrees |
| Velocity of Launch | 3.869√R | $3.869\sqrt{(R+S)\tan\theta}$ | $\frac{2.736R}{\sqrt{h_0}}$ | 5.4716 $\left\{-\mu \sqrt{h_o} + \sqrt{\mu (\mu h_0 + R + S)}\right\}$ | MPH |
| Horizontal Distance in Air | R | R | R | R | Feet |
| Horizontal Distance on Ground | 0 | S | 0 | S | Feet |
| Maximum Height Of Trajectory | 0.25R | $\left(\frac{\mathbf{R}+\mathbf{S}}{2}\right)$ $\tan\theta\sin^2\theta$ | h _o | h _o | Feet |
| Distance to Max. Height | 0.50R | 0.50R | 0 | 0 | Feet |
| Time to Max. Height | $0.7071\sqrt{\frac{R}{g}}$ | $\sin\theta \sqrt{\left(\frac{R+S}{g}\right)}\tan\theta$ | 0 | 0 | Seconds |
| Time in Air | $1.4142\sqrt{\frac{R}{g}}$ | $2\sin\theta \sqrt{\left(\frac{R+S}{g}\right)\tan\theta}$ | $\sqrt{\frac{2h_0}{g}}$ | $\sqrt{\frac{2h_0}{g}}$ | Seconds |
| Total Time in Motion | $1.4142\sqrt{\frac{R}{g}}$ | $\left(2\sin\theta + \frac{1}{\mu}\right)\sqrt{\left(\frac{R+S}{g}\right)\tan\theta}$ | $\sqrt{\frac{2h_0}{g}}$ | $\sqrt{\frac{2(\mu h_0 + R + S)}{\mu g}}$ | Seconds |

Table 13 Summary of Analytical Relationships for Occupant Trajectory

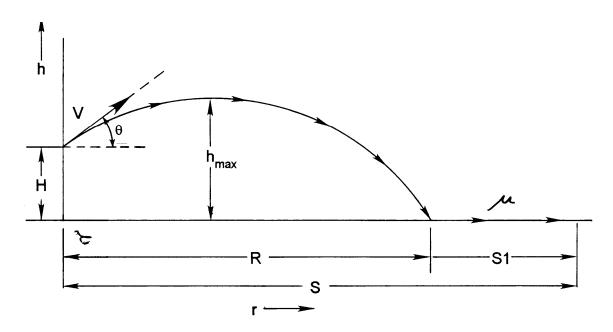


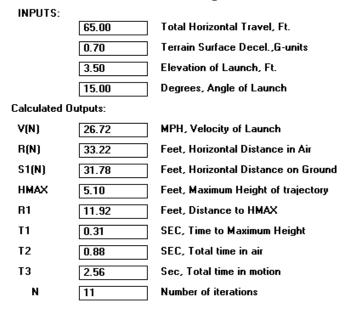
Figure 71 General Case Launch Analysis

LAUNCH Routine.

The LAUNCH routine, developed by McHenry Software, Inc., constitutes a general-case analytical approach, as depicted in **Figure 71**. An iterative solution procedure is used. The output format which is depicted in **Figure 72** *and* **Figure 73**, includes the option of either (a) specifying a launch angle or (b) permitting the LAUNCH routine to find the optimum angle (i.e., to determine the minimum speed for a given travel distance. The results of sample applications are also depicted in **Figure 74**.

| | L | AUNCH Program |
|--------------|---------|-------------------------------------|
| INPUTS: | | |
| | 65.00 | Total Horizontal Travel, Ft. |
| | 0.70 |] Terrain Surface Decel.,G-units |
| | 3.50 | Elevation of Launch, Ft. |
| Calculated O | utputs: | |
| Theta(N) | 32.21 | Degrees, Angle of Launch |
| V(N) | 25.22 | MPH, Velocity of Launch |
| R(N) | 43.26 | Feet, Horizontal Distance in Air |
| S1(N) | 21.74 | Feet, Horizontal Distance on Ground |
| HMAX | 9.54 | Feet, Maximum Height of trajectory |
| R1 | 19.17 | Feet, Distance to HMAX |
| T1 | 0.61 | SEC, Time to Maximum Height |
| T2 | 1.38 | SEC, Total time in air |
| Т3 | 2.77 | Sec, Total time in motion |
| N | 12 | Number of iterations |

Figure 72 Sample Launch Output Format for optimum launch angle



LAUNCH Program

Figure 73 Sample Launch Output Format for 15° launch angle

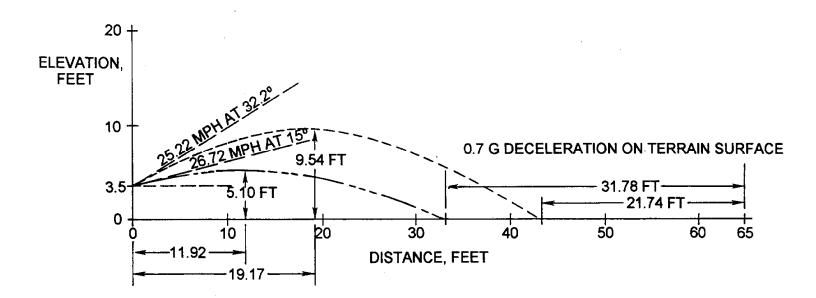


Figure 74 Results of Sample Applications of Launch